Time-dependent deformation in rocks

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Time-dependent deformation in rocks

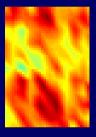
- Phenomenology of brittle-ductile transition in porous Rocks: Transition of failure mode from brittle faulting to cataclastic flow/compaction bands.
- Damage evolution and strain localization.
- □ Time-dependent deformation and failure in rocks: time-dependent failure/compaction.

effective mean stress: $(\sigma_1+2\sigma_3)/3 - P_p$

P*: grain crushing pressure

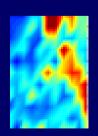
C*: onset of shear-enhanced compaction

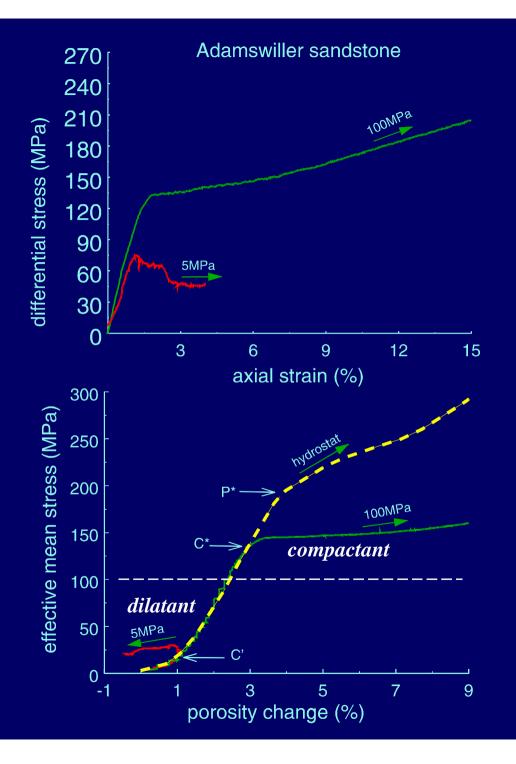




C': onset of dilatancy







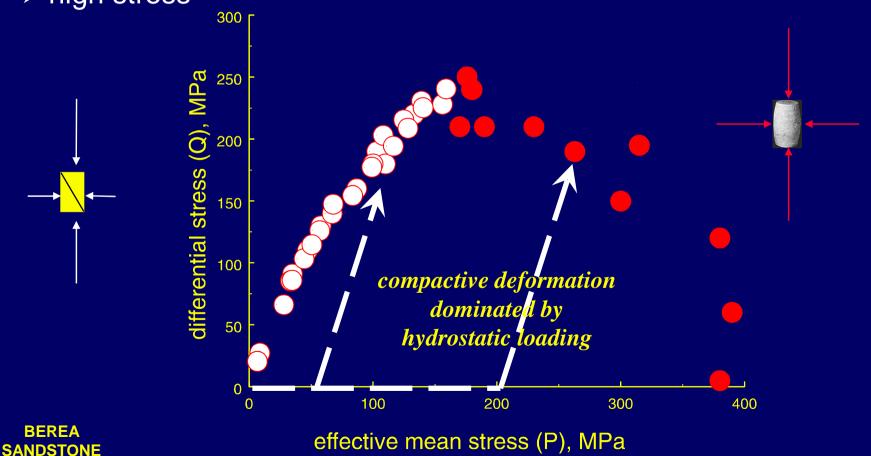
Brittle-Ductile Transition and Failure Modes

brittle fracture: shear localization

- dilatancy
- > low confinement
- high stress

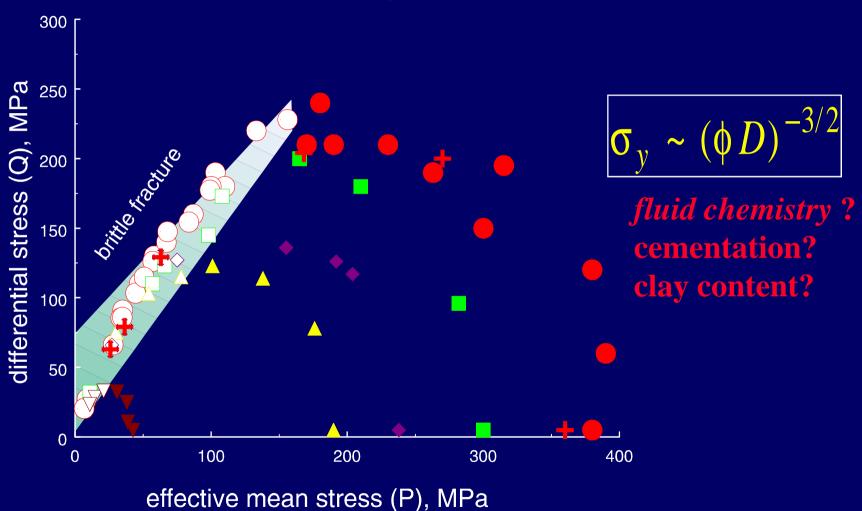
compactive yield: bulk failure

- shear-enhanced compaction
- high confinement
- low deviatoric stresses

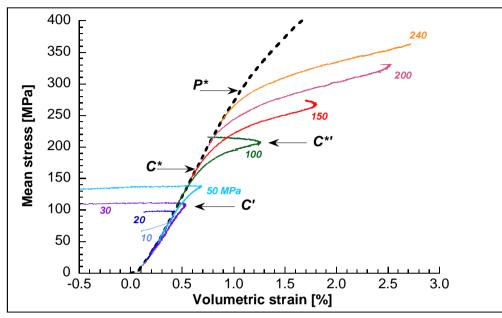


COMPACTIVE YIELD ENVELOPE:

an elliptical cap with yield stresses dependent on porosity ϕ and grain size D



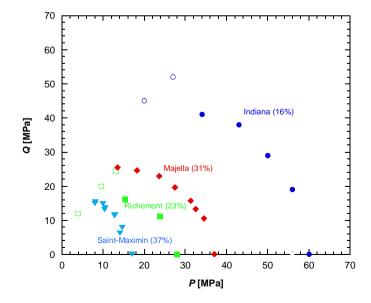
Brittle-ductile transition in porous limestones

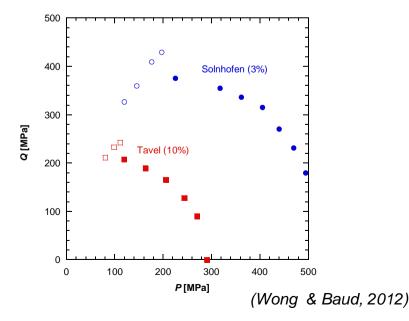


(Tavel limestone, porosity 10%, Vajdova, Baud and Wong, 2004)

- phenomenology similar for limestones with porosities 3-18%
- brittle-ductile transition qualitatively similar to porous sandstone

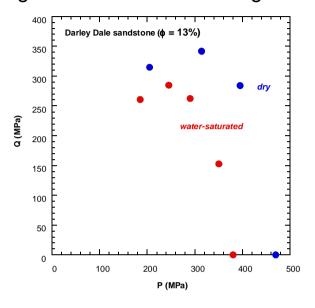
C' onset of dilatancy
C* onset of shear-enhanced compaction
C*' transition from shear-enhanced
compaction to dilatancy

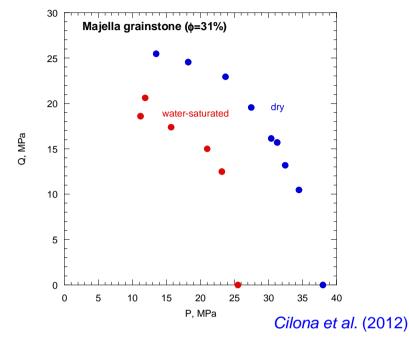


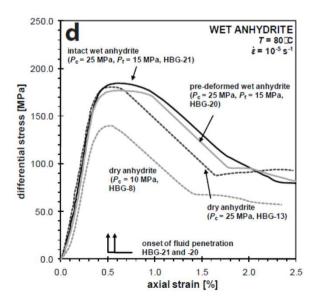


Fluid weakening: short-term effect

significant water weakening in sandstone and limestone









■ Mechanical data on brittle strength of anhydrite saturated with CO₂ and subjected to a static pore pressure show that the short-term chemical effect on strength is relatively small.

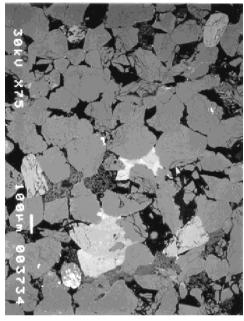
Hangx, Spiers & Peach (2010)

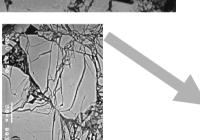
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Microstructure: brittle regime



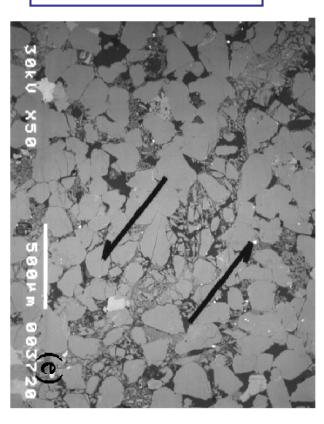




Stress-induced damage:

- spatial clustering
- anisotropic cracking

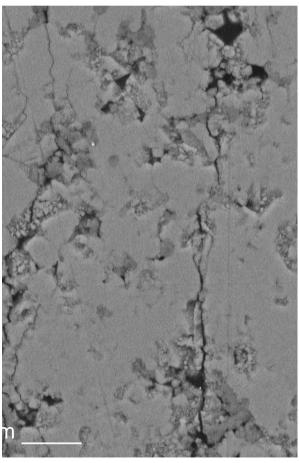
Berea sandstone $(P_{eff} = 10 \text{ MPa})$



Shear localization

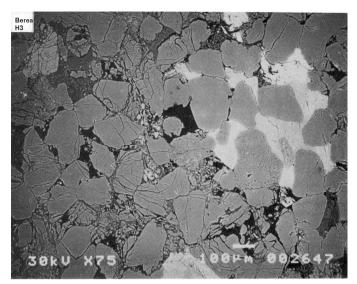
Tavel limestone: Onset of dilatancy

pore emanated-microcracks

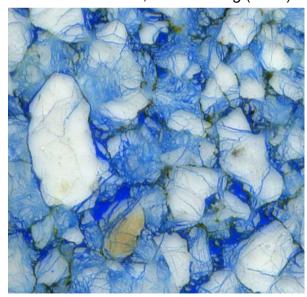


(Vajdova et al., 2004)

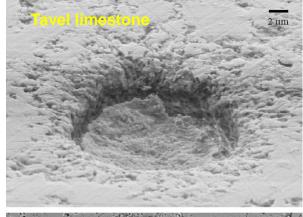
Hydrostatic Loading: Cataclastic pore collapse/grain crushing

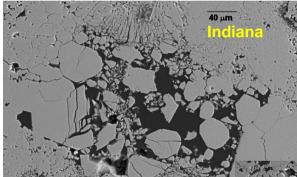


Berea sandstone Menéndez, Zhu & Wong (1996)



Boise sandstone Wong & Baud (2012)





SANDSTONE: stress
concentration at grain
contact → Hertzian
fracture → intragranular
cracking → grain crushing
→ pore collapse

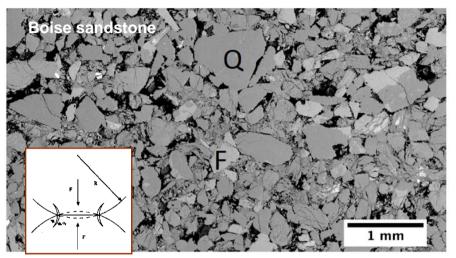
LIMESTONE:

stress
concentration at
periphery of
equant pore →
localized
cataclastic
damage →
spalled fragments
fall into the void
→ pore collapse

Triaxial Loading: compaction bands/homogeneous compaction

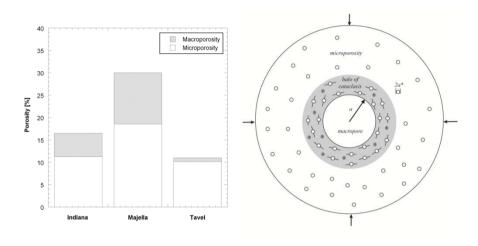
SANDSTONE

•Cataclastic flow: Hertzian cracking (Cheung et al., 2012)

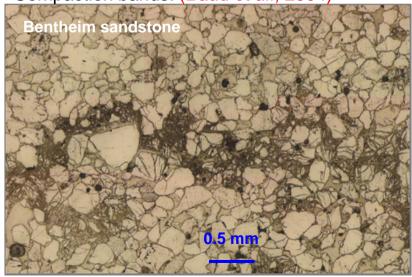


LIMESTONE

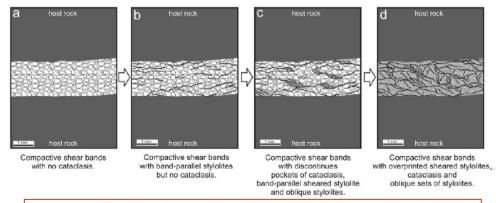
•Cataclastic pore collapse (Zhu et al., 2010)



•Compaction bands: (Baud et al., 2004)



•Compaction localization in carbonates



The role of deformation bands, stylolites and sheared stylolites in fault development in carbonate grainstones of Majella Mountain, Italy

Emanuele Tondi a,*, Marco Antonellini b, Atilla Aydin b, Leonardo Marchegiani a, Giuseppe Cello a

Journal of Structural Geology 28 (2006) 376-391

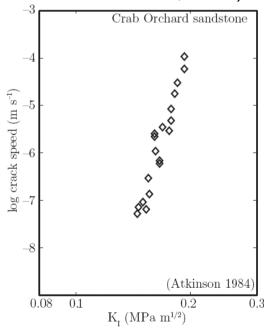
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Time-dependent brittle failure: subcritical cracking and creep

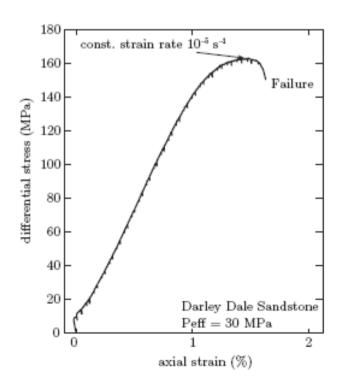
- The presence of a fluid phase in porous rocks not only affects the mechanical behaviour of rock, but also allows chemical rock-fluid interactions to occur.
- Subcritical crack processes such as stress corrosion [Anderson and Grew, 1977;
 Atkinson, 1984, Atkinson and Meredith, 1987; Costin, 1987] introduce a time-dependence that allows rock to fail at lower stress over extended time.
- Stress corrosion describes the reactions that occur preferentially between a chemically active pore fluid, most commonly water, and the strained atomic bonds close to crack tips.
 - slow crack propagation:

•extremely sensitive to stress (*Atkinson & Meredith*, 2007)



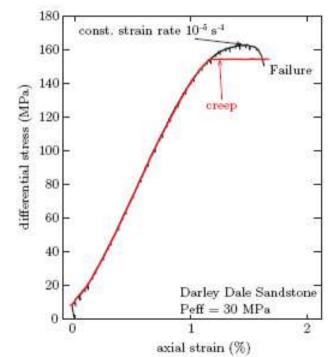
Triaxial experiments

- water-saturated samples, drained conditions ($P_p = 10 \text{ MPa}$)
- sample size: 100 mm x 40 mm
- acoustic emission location
- internal furnace
 - conventional triaxial experiment: imposed fast strain rate (10⁻⁵/s) until failure
 - large quantity of data on many rocks



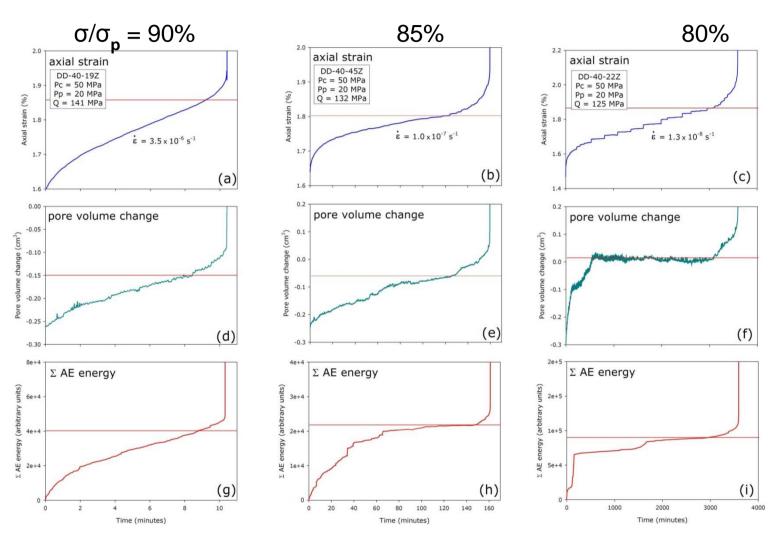


- creep tests: imposed constant stress
- strain rates between 10⁻⁹/s and 10⁻⁵/s
- paucity of data



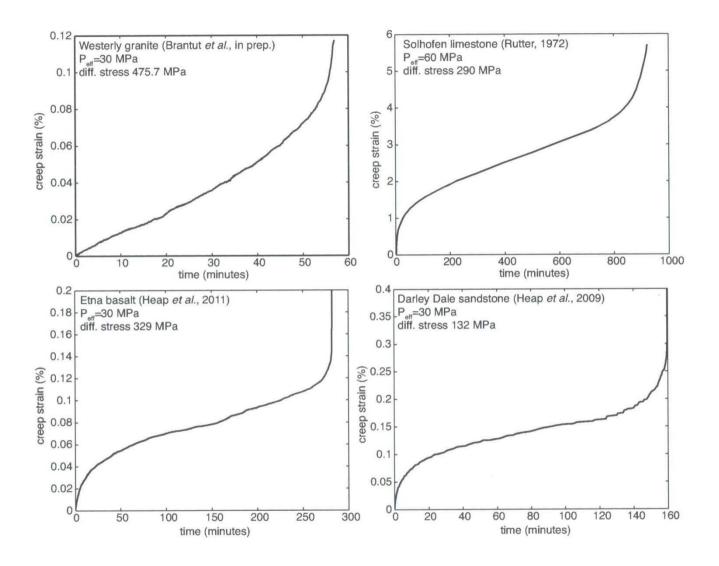


Creep experiments (static fatigue): sandstone



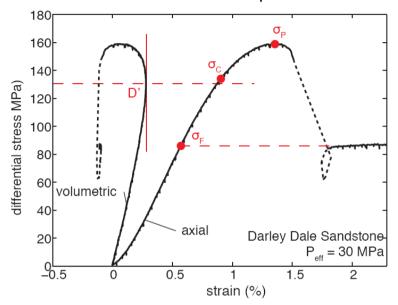
- damage proxies: strain, porosity, AE
- critical level of damage

Brittle creep: same phenomenology in other rock types

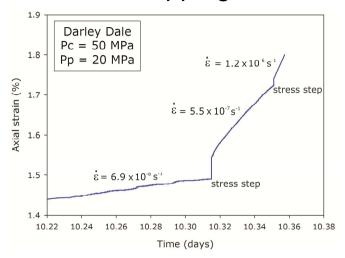


Creep experiments

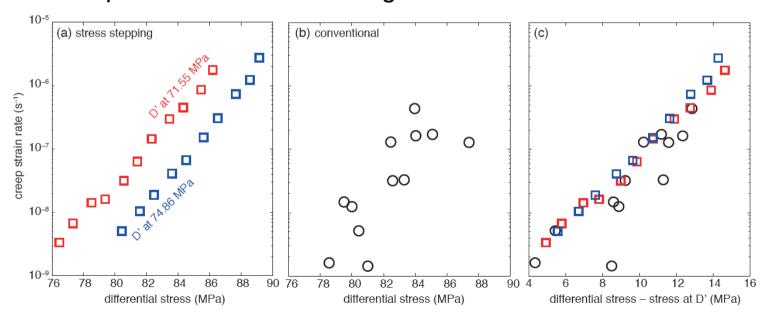
•creep between D' and σ_p

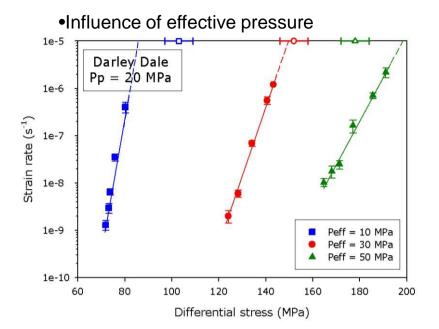


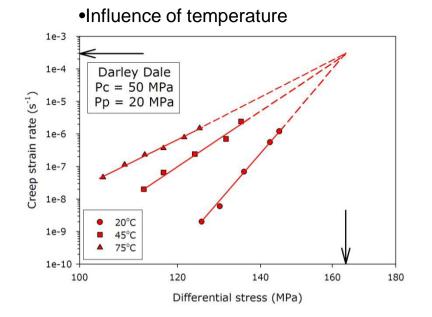
stress stepping methodology



• importance of initial damage







Using a simple uniaxial strain model for Darley Dale sandstone at 1 km depth

Expected changes in creep strain rate over a depth of 2km Experimental data on Darley Dale sandstone suggest:

- Increase by 2 x 10³ due to the increase in temperature
- Decrease by 3 x 10³ due to the increase effective mean stress
- Increase by 10³ due to increase in differential stress

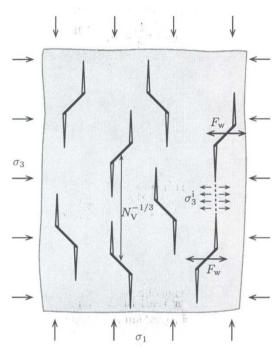
The effects of the well constrained parameters (P_{eff}, T) almost exactly balanced. This suggests that the key parameter controlling the strain rate of brittle creep in the crust is the **differential stress**, and this will vary significantly with tectonic regimes. Interpretation of local creep rates would therefore require a specific knowledge of the local stress regime and its evolution with depth.

Heap et al., GRL (2009)

•Micromechanical model for brittle creep

(Brantut, Baud, Heap, Meredith, JGR, 2012)

• Starting geometry (Sammis & Ashby, 1990)

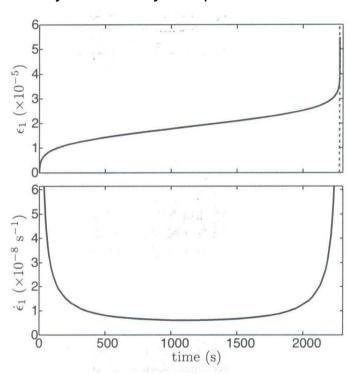


• Subcritical crack growth (Charles):

$$\frac{dl}{dt} = \dot{l}_{0} \left(K_{I} / K_{IC} \right)^{n}$$

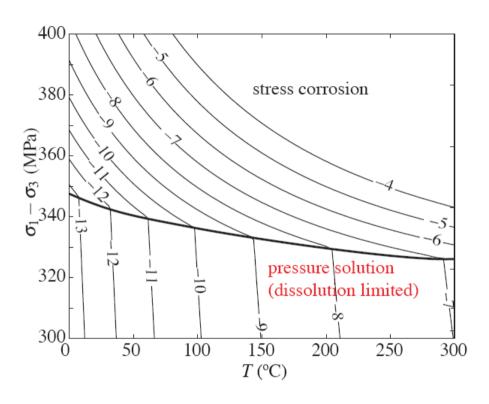
Microcrack interactions

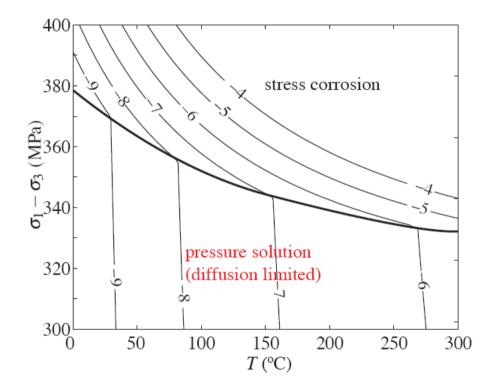
• The model reproduces the macroscopic phenomenology and in particular primary, secondary and tertiary creep.



$$\dot{\mathcal{E}} \propto \left[1 - k \frac{\sigma_1^{peak} - \sigma_1}{K_{IC} \sqrt{\pi a}} \right]^{n+1}$$

Deformation maps: sandstone





PS strain rate calculated from model of Niemeijer et al. (2002) for dissolution-limited creep.

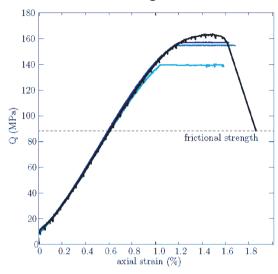
PS strain rate calculated from model of Rutter (1983) for diffusion-limited creep.

It therefore appears that PS is likely too slow to explain our experimental data at ambient T.

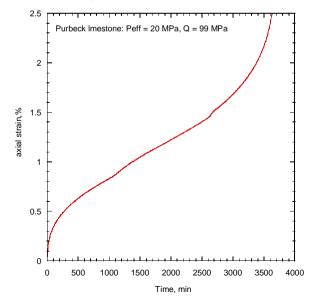
(Brantut et al., JGR, 2012)

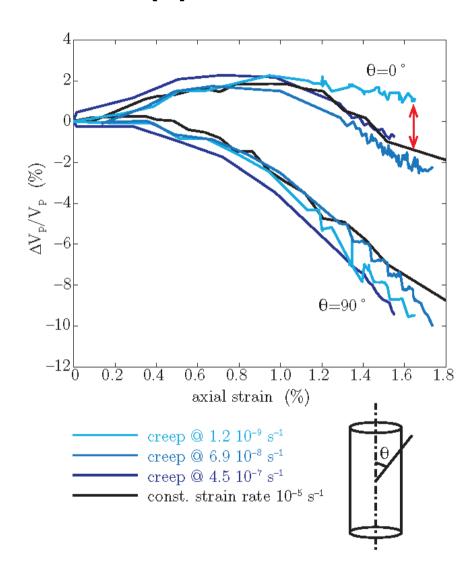
Other mechanism(s)?

• sandstone: less cracking at slow strain rates

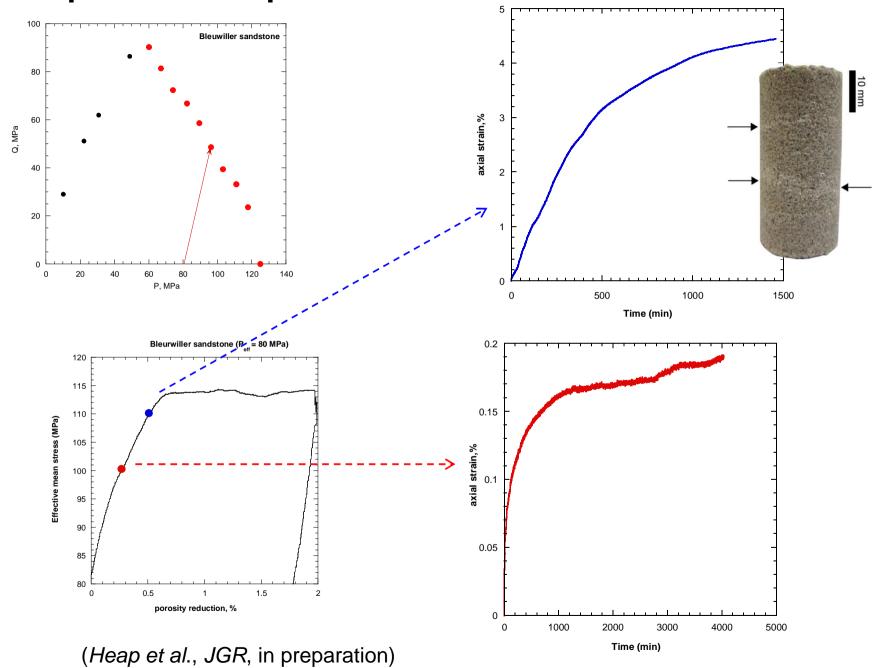


• limestone: larger amount of strain





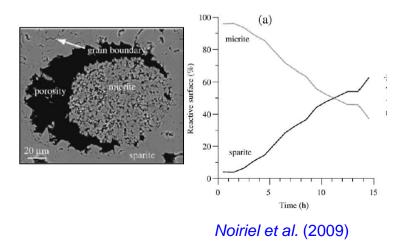
Time-dependent compaction: sandstone



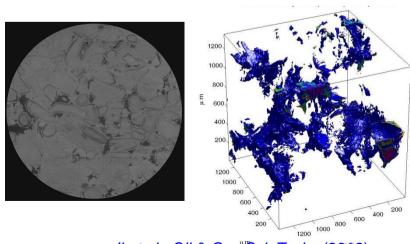
Conclusions and perspectives

- Experiments on sandstone enabled to quantify the influence of in situ conditions on brittle creep.
- The experimental data suggest that the creep strain rate at depth is controlled by the differential stress.
- A simple micromechanical model explains how brittle creep operates and is in good quantitative agreement with data.
- Useful for predictions of long term strength of the brittle crust.
- Current work on time-dependent deformation in limestone and compactant creep.

Upper Miocene limestone from Mallorca (~16%)



Multiscale X-ray CT imaging



Ji et al., Oil & Gas[™]Sci. Tech. (2012)